# University of Asia Pacific Department of Civil Engineering <br> Final Examination Spring 2018 Program: B.Sc. in Civil Engineering 

## QUESTION 1 [20 MARKS]

a) State fundamental assumptions to analyze statically indeterminate frame structure for gravity (vertical) load using approximate method and lateral load using Cantilever Method. [2+2]
b) Formulate the equation to calculate deflections of truss and frame using Virtual Work Method.
c) Explain the basic principle of force method to analyze statically indeterminate beam and frame.
d) Draw the qualitative influence lines of shear forces $\mathrm{V}_{\mathrm{C}(\text { Leff) }}, \mathrm{V}_{\mathrm{C} \text { (Right) }}$ and bending moments $M_{A}, M_{B}$ of the beam shown in Figure 1(a).
e) State the parameters that influence the joint moment distribution factor. Formulate the equation to calculate moment distribution factors at joint $B$ of the structure shown in Figure 1(b).
[2+2]


## QUESTION 2 [20 MARKS]

Figure 1(b)
a) A frame of reinforced concrete building is shown in Figure 2 (a). All beams of the frame are carrying $40 \mathrm{kN} / \mathrm{m}$ floor (vertical) load. Analyze the structure using approximate method to get bending moment diagram (BMD) of ground floor roof beams.
b) The frame shown in Figure 2(a) is subjected to lateral load due to earthquake. In general, ground floor columns are more critical in bending moment compared to top floor columns. Justify the statement through analysis of the structure using Portal or Cantilever Method. The cross sections of all columns are same.
c) A frame of portal mill of industry building is subjected to 48 kN lateral load as shown in Figure 2(b). Analyze the frame for bending moment of columns.


Figure 2(a): Frame of residential building


Figure 2(b): Frame of portal mill

## QUESTION 3 [20 MARKS]

a) A steel floor truss of industry building is carrying vertical load as shown in Figure 3(a). Apply Virtual Work Method to obtain maximum vertical deflection of the truss.
[Given: Cross-sections of members are $1200 \mathrm{~mm}^{2}$, Modulus of elasticity of steel is 200 GPa].
b) A reinforced concrete slab ABC is carrying $15 \mathrm{kN} / \mathrm{m}$ floor load as shown in Figure 3(b). The thickness of slab is 0.2 m and width is 1 m . Modulus of elasticity of concrete is 30,000 $\mathrm{N} / \mathrm{mm}^{2}$. Apply Virtual Work Method to calculate deflection at C.


Figure 3(a): Floor truss


Figure 3(b): RC slab

## OUESTION $4[20$ MARKS]

a) A bill board steel truss structure has joint forces due to wind as shown in Figure 4(a). Analyze the truss using force method.
[Given: Cross section of all members is $1200 \mathrm{~mm}^{2}$, Modulus of elasticity of steel is 200 GPa].


Figure 4(b): RC continuous beam

Figure 4(a): Truss of bill board
b) Analyze the reinforced concrete continuous beam ABC shown in Figure 4(b) for bending moment and shear force using Moment Distribution Method. EI is constant.
[Given: Fixed end moment for uniformly distributed load is $\mathrm{wL}^{2} / 12$, for concentrated load (at middle of beam) is PL/8]
[10]

## QUESTION 5 [20 MARKS

a) A brick-reinforced concrete building structure is shown in Figure 5(a). The beam ABC is carrying $40 \mathrm{kN} / \mathrm{m}$ design load (uniform). The size of the beam is $0.25 \mathrm{~m} \times 0.8 \mathrm{~m}$. The element BD could be RC column or brick wall. As a structural engineer select the appropriate structural system to have lower sagging bending moment of beam BC and justify your selection through comparative analysis of the structure using Moment Distribution Method. The size of BD RC column is $0.4 \mathrm{~m} \times 0.4 \mathrm{~m}$. Assume pin connection at beam-brick wall joint.
[10]
b) A reinforced concrete frame of porch is carrying 10 kN lateral load due to wind as shown in Figure 5(b). The maximum allowable lateral deflection at joint $C$ is 10 mm . Select the appropriate size of column AB to maintain the maximum deflection at joint C and justify your selection through analysis of the frame using Virtual Work Method. Assume the section of beam BC is 0.25 mx 0.4 m . Modulus of elasticity of concrete is $30,000 \mathrm{~N} / \mathrm{mm}^{2}$.


Figure 5(a): Frame of brick-concrete structure


Figure 5(b): Prototype of porch

# University of Asia Pacific <br> Department of Civil Engineering <br> Final Examination Spring 2018 <br> Program: B.Sc. in Civil Engineering 

Course Title: Design of Concrete Structures II
Course Code: CE 317
Time: 3 (Three) hours
Full Marks: 100
Assume reasonable values for any missing data. Symbols used have their usual meanings. [Use $f_{c}^{\prime}=30 \mathrm{~N} / \mathrm{mm}^{2}(4 \mathrm{ksi})$ and $f_{y}=415 \mathrm{~N} / \mathrm{mm}^{2}$ (60 ksi) for all design]

## QUESTION 1 [20 MARKS]

a. Explain why the factors $\phi$ and $\alpha$ are used for column design.
b. Why are special reinforcements needed at the corners of a two way slab system? Discuss the possible special arrangements.
c. State the critical parameters of punching shear to control the thickness of foundation.

Show the layout of pile caps of 4 piles and 5 piles, diameter of friction pile is 400 mm . [3+2]
d. Discuss how to check stability of cantilever type reinforced concrete retaining wall.

State the basic principles of methods of pre-stressing.

## QUESTION 2 [20 MARKS]

a. A beam-supported interior slab panel is carrying loads of 30 psf from floor finish and 50 psf from random wall. Calculated reinforcement (in USD) in short span was found to be \#3 @ $8.25^{\prime \prime} \mathrm{c} / \mathrm{c}$ (bottom), alt ckd $+2 \# 3$ extra top as shown in Figure 1. Thickness of the slab was found to be $4.5^{\prime \prime}$. Calculate the live load that can be carried by the slab panel. Use Moment Co-efficient method.


Figure 1: Details of slab


Figure 2: Details of flat slab
b. Calculate the design moments of the panel "D" of a flat slab (Figure 2) of size $18 \mathrm{~B} \times 16^{\prime} \mathrm{c} / \mathrm{c}$ (supported on $12^{\prime \prime} \times 12^{\prime \prime}$ edge beams), if it carries floor finish $=30 \mathrm{psf}$, random wall $=50 \mathrm{psf}$, live load $=60 \mathrm{psf}$.

## QUESTION 3 [20 MARKS]

a. Design a (i) round spiral and a (ii) square column to support an axial dead load of 200 k and live load of 300 k . Initially assume $2 \%$ longitudinal steel.
b. A $12^{\prime \prime} \times 18^{\prime \prime}$ column is reinforced with six \#9 bars as shown in Figure 3. Determine,
(i) the load $\mathrm{P}_{\mathrm{b}}$, Moment $\mathrm{M}_{\mathrm{b}}$ and corresponding eccentricity $\mathrm{e}_{\mathrm{b}}$ for balanced failure
(ii) the load and moment for a representative point in the compression failure region of the interaction diagram (with $2.5^{\prime \prime}$ cover on all sides).


Figure 3: Section of column


Figure 4: Layout plan of column

## QUESTION 4 [20 MARKS]

a. The interior column ( $400 \mathrm{~mm} \times 400 \mathrm{~mm}$ ) as shown in Figure 4 of 5-storeyed car park (flat slab structure) is supported by isolated footing. The thickness of flat slab is 250 mm and each floor height is 3.3 m . The live load of car park is $2.5 \mathrm{kN} / \mathrm{m}^{2}$ and the bearing capacity of soil is $150 \mathrm{kN} / \mathrm{m}^{2}$. Design the footing with optimal depth considering all critical parameters. Assume required data for design. Unit weight of concrete is $24 \mathrm{kN} / \mathrm{m}^{3}$.
b. An interior column ( $400 \mathrm{~mm} \times 400 \mathrm{~mm}$ ) of a 9 storeyed academic building is supported by bore pile foundation. The dead and live loads of the foundation are 2400 kN and 800 kN respectively. There is an option to select the piles i.e. 500 mm pile of 900 kN capacity or 400 mm pile of 750 kN capacity. Select the appropriate pile to have minimum depth of pile cap and justify your selection through checking of punching shear. Design the pile cap with your selected pile. Assume required data for design.

## QUESTION 5 [20 MARKS]

a. Two interior columns ( $400 \mathrm{~mm} \times 400 \mathrm{~mm}$ ) as shown in Figure 5 of RC structure is supported by combined footing. The dead and live loads of each column are 1200 kN and 350 kN respectively. The bearing capacity of soil is $120 \mathrm{kN} / \mathrm{m}^{2}$. Design the footing for long span bottom reinforcements only. Assume the effective depth of the footing is 500 mm .


Figure 5: Layout of columns for combined footing
b. A settling tank of mini hydro power plant is constructed with retaining wall as shown in Figure 6. The density of water is $1000 \mathrm{~kg} / \mathrm{m}^{3}$. Design the wall for moment. Assume the required thickness of wall, cover is 75 mm and diameter of main reinforcement is 16 mm . As per ACI, the basic span depth ratio of cantilever slab is 10 .
c. A simply supported 8 meter span pre-stress concrete beam is carrying $15 \mathrm{kN} / \mathrm{m}$ live load. The section of the rectangular beam is $400 \mathrm{~mm} \times 200 \mathrm{~mm}$. A straight tendon is provided at an eccentricity of 75 mm below the centroid of the section. "The eccentricity of tendon reduces pre-stressing force and compressive stress on section", Justify the statement through analysis of the beam for maximum bending moment at mid-span.

## APPENDIX

## Co-efficient Method:

$\mathrm{Ma}=\mathrm{C}_{\mathrm{a}} \mathrm{w}_{\mathrm{u}} \mathrm{la}^{2}$
$\mathrm{Mb}=\mathrm{C}_{\mathrm{b}} \mathrm{w}_{\mathrm{u}} \mathrm{lb}^{2}$
Thickness $\mathrm{h}=\mathrm{P} / 180 \geq 3.5, \mathrm{P}=$ panel perimeter
Shear strength of the slab, $\varphi V_{c}=2 \sqrt{f_{c}^{\prime}} b d$

$$
\mathrm{d}=\sqrt{\frac{M_{\mathrm{k}}}{}} \sqrt{\phi \rho_{y}\left(1-0.59 \rho \frac{f_{y}}{f_{c}}\right)} \quad \text { Here } \rho=\rho_{\max }=0.75 \rho_{y}=0.75 * 0.85 * \beta_{1} \frac{f_{c}^{\prime}}{f_{y}} \cdot \frac{87000}{87000+f_{y}}
$$

As $=\left(f_{c} / f_{v}\right)\left[1-v\left\{1-2 M_{n} /\left(f_{c} b d^{2}\right)\right\}\right] b d$

## Direct Design Method:

Minimum thickness of Flat Slab

| Exterior Panels <br> without Edge Beams | Exterior Panels <br> with Edge Beams | Interior Panels |
| :---: | :---: | :---: |
| $L_{n} / 33$ | $L_{n} / 36$ | $L_{n} / 36$ |

For reinforcements with fy $\neq 40 \mathrm{ksi}$, the tabulated values are to be multiplied by $(0.8+\mathrm{fy} / 200)$.
$M_{o}=w_{n} L_{2} L_{n}^{2} / 8 ; M_{u}^{(-)}=0.65 M_{o} ; M_{u}^{(+)}=0.35 M_{o}$
Distribution Factors applied to Static Moment $\mathrm{M}_{0}$ for Positive and Negative Moments

| Position of <br> Moment | Ext Edge <br> unrestrained <br> (a) | Slab with beams between all <br> supports <br> $(\mathrm{b})$ | No beam between interior supports |  | Exterior Edge fully <br> restrained <br> (e) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Exterior $M^{(-)}$ | 0.00 | 0.16 | Without edge <br> beam (c) | With edge <br> beam (d) | (e) |
| Interior $M^{(-)}$ | 0.75 | 0.70 | 0.26 | 0.30 | 0.65 |
| $M^{(+)}$ | 0.63 | 0.57 | 0.70 | 0.70 | 0.65 |

$$
\begin{aligned}
& \alpha=E_{c b} I_{b} / E_{c s} I_{s} \quad \beta_{t}=E_{c b} C / 2 E_{c s} I_{s} \quad C=\sum(1-0.63 x / y) x^{3} y / 3 \\
& \% \text { of Exterior } M^{(t)} \text { supported by Column Strip }=100-10 \beta_{t}+12 \beta_{t}\left(\alpha_{1} L_{y} / L_{1}\right)\left(1-L_{2} / L_{1}\right)
\end{aligned}
$$

$$
\% \text { of } M^{(-)} \text {supported by Column Strip }=60+30\left(\alpha_{1} L_{2} / L_{1}\right)\left(1.5-L_{2} / L_{1}\right)
$$

$$
\% \text { of Interior } M^{-1} \text { supported by Column Strip }=75+30\left(\alpha_{1} L_{2} / L_{1}\right)\left(1-L_{2} / L_{1}\right)
$$

For slabs without beams between supports $\left(\alpha_{1}=0\right)$ and without edge beams ( $\beta t=0$ ), the portion of negative moments in column strip is simply $100 \%$ and $75 \%$ for exterior and interior supports, respectively, and portion of positive moment in column strip is simply $60 \%$.
Punching shear capacity $V_{c}=4 \sqrt{ } f_{c}^{\prime} b_{o} d$
Short Column:
Axial Capacity $P_{u}=\alpha \phi A_{g}\left[0.85 f_{c}{ }^{\prime}+\rho_{s}\left(f_{y}-0.85 f_{c}{ }^{\prime}\right)\right]$

$$
\begin{aligned}
c & =c_{b}=d \frac{\epsilon_{u}}{\epsilon_{u}+\epsilon_{y}} \quad f_{s}=\epsilon_{u} E_{s} \frac{d-c}{c} \leq f_{y} \quad f_{s}^{\prime}=\epsilon_{u} E_{s} \frac{c-d^{\prime}}{c} \leq f_{y} \quad C=0.85 f_{c}^{\prime} a b \\
P_{n} & =0.85 f_{c}^{\prime} a b+A_{s}^{\prime} f_{s}^{\prime}-A_{s} f_{s} \\
M_{n} & =P_{n} e=0.85 f_{c}^{\prime} a b\left(\frac{h}{2}-\frac{a}{2}\right)+A_{s}^{\prime} f_{s}^{\prime}\left(\frac{h}{2}-d^{\prime}\right)+A_{s} f_{s}\left(d-\frac{h}{2}\right) \\
K_{n} & =\frac{P_{u}}{\phi f_{c}^{\prime} A_{g}} \quad R_{n}=\frac{M_{u}}{\phi f_{c}^{\prime} A_{g} h}
\end{aligned}
$$

CE 317 Formulae 2: In SI unit
Flexural shear capacity of normal concrete: $V_{c}=0.17 \sqrt{f_{c}^{\prime}} b_{w} d$
Punching shear capacity of normal concrete: $V_{p}=0.33 \sqrt{f_{c}^{\prime}} u d$
Minimum flexural reinforcement: $A_{s, \text { min }}=\frac{0.25 \sqrt{f_{c}^{\prime}}}{f_{y}} b_{w} d \geq \frac{1.4 b_{w} d}{f_{y}}$


| Case 1 |
| :---: |

## 



Case 4





Fig. 1.5: Moment coefficients for different support conditions

# University of Asia Pacific Department of Civil Engineering Final Examination Spring 2018 <br> Program: B.Sc. Engineering (Civil) 

Course Title: Environmental Engineering II
Time: 3 hours

Course Code: CE 333
Full Marks: 100

## There are six (6) questions. Question no. 6 is compulsory. Answer Question no. 6 and any four (4) from the rest. Assume any missing data.

1. (a) Differentiate between cistern flush and pour flush toilets.
(b) Explain the major pollutant removal mechanisms in a septic tank system. How water turbulence influences removal performance in a septic tank?
(c) How oil and grease are removed from wastewater?
(d) A settling analysis is run on a type 1 suspension. The column is 2 m deep, and the data set are given below. Compute the removal efficiency in a settling basin with a load of $20 \mathrm{~m} / \mathrm{d}$.

| Time, min | 0 | 60 | 80 | 100 | 130 | 200 | 240 | 420 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conc., $\mathrm{mg} / \mathrm{L}$ | 400 | 250 | 160 | 130 | 110 | 90 | 50 | 5 |

2. (a) With necessary assumptions derive the equation $L_{t}=L_{0} e^{-k t}$ for quantifying BOD concentration of water/wastewater.
(b) Show schematic diagrams of a completely mixed reactor with: wasting of sludge from aeration tank and wasting from return sludge line. How MLSS and MLVSS are formed in an aeration tank?
(c) With engineering diagrams explain tapered aeration and pure oxygen activated sludge systems.
(d) Calculate: (i) efficiency (ii) dimensions and (iii) sludge wasting flow of aeration tanks employing the following data set. Use the provided equations if required.
```
> Average design flow }=0.50\mp@subsup{\textrm{m}}{}{3}/\textrm{s
> Influent }\mp@subsup{\textrm{BOD}}{5}{}\mathrm{ concentration=450 mg/L
> Influent TSS concentration=250 mg/L
> Effluent BOD concentration=20 mg/L
 Effluent TSS concentration=20 mg/L
Sludge age, }\mp@subsup{0}{c}{}=8\textrm{d
> MLVSS=2000 mg/L
VSS/TSS=0.7
TSS concentration in RAS }=10000\textrm{mg}/\textrm{L
> Y=0.5 mg VSS/mg BOD }\mp@subsup{}{5}{},\mp@subsup{\textrm{k}}{\textrm{d}}{}=0.06/\textrm{d
> - BOD 
* }\mp@subsup{\textrm{BOD}}{5}{}\mathrm{ removal in primary clarifiers=35%
T TSS removal in primary clarifiers=65%
```

$>$ Specific gravity of primary sludge is 1.05 , with solid content $4.4 \%$
$>$ Oxygen consumption is 1.42 mg per mg of cell oxidized
Equations: $\quad V=\frac{\theta_{c} Q Y\left(S_{o}-S\right)}{X\left(l+k_{d} \theta_{c}\right)} \cdots \quad \theta_{c}=\frac{V X}{Q_{w a} X+Q_{e} X_{e}}$
3. (a) Explain cell growth curve of bacteria.
(b) What is the main difference between CSTR and plug flow reactors?
(c) With necessary diagrams briefly describe operational principles of a rotating biological contactor reactor.
(d) The $\mathrm{BOD}_{5}$ of a wastewater is $400 \mathrm{mg} / \mathrm{L}$ at $20^{\circ} \mathrm{C} . \mathrm{k}$ at $20^{\circ} \mathrm{C}$ is 0.20 per day. Determine the $\mathrm{BOD}_{8}$ of the sample at $10^{\circ} \mathrm{C}$.
4. (a) How sludge dewatering is achieved employing drying beds?
(b) Briefly explain ammonication, nitrification and denitrification processes that often control nitrogen removals in a biological reactor.
(c) Write short notes on: (i) Bardenpho system for nitrogen removals; (ii) Simultaneous phosphorus precipitation and (iii) The three stage Phoredox ( $\mathrm{A}^{2} / \mathrm{O}$ ) system for phosphorus removal.
5. (a) Enlist the advantages and disadvantages of stabilization ponds.
(b) How DO and pH concentration fluctuates with change of sunlight duration in a facultative pond?
(c) How effluent recirculation and aeration enhance pollutant removals in a vertical flow wetland?
(d) Explain pollutant removal differences between horizontal flow and floating treatment wetlands.
6. As an environmental engineer you have been assigned to propose wastewater treatment plant diagrams for two industries. Effluent wastewater characteristics of these industries are summarized in the following table. Propose treatment flow diagrams for industry 1 which will include activated sludge process and stabilization pond/constructed wetland systems for industry 2.

|  | Unit | Concentration value |  |
| :---: | :---: | :---: | :---: |
|  |  | Industry 1 | Industry 2 |
| pH | --- | 7.3 | 5 |
| DO | $\mathrm{mg} / \mathrm{L}$ | 0.5 | 0.8 |
| Solids |  | 2000 | . 500 |
| $\mathrm{NH}_{4}-\mathrm{N}$ |  | 15 | 120 |
| $\mathrm{NO}_{3}-\mathrm{N}$ |  | 5 | 20 |
| TN |  | 30 | 180 |
| P |  | 0.7 | 12 |
| $\mathrm{BOD}_{5}$ |  | 4500 | 350 |
| COD |  | 9000 | 600 |

# University of Asia pacific Department of Civil Engineering Final Examination Spring 2018 Program: B.Sc. Engineering (Civil) 

Course Title: Transportation Engineering I (Transport and Traffic Design) Time: 3 Hours

Course Code: CE 351
Full Marks: 150

There are six questions. Answer five of them.

1. a) Compile different types of problems caused by on-street parking in Dhaka city.
b) Determine the AADT for the following data. Data collection was conducted on Tuesday in August. MEF for August is 0.578 .

| Hour | Volume |
| :---: | :---: |
| 7:00-8:00 a.m. | 1300 |
| 8:00-9:00 a.m. | 1450 |
| 9:00-10:00 a.m. | 1200 |
| 10:00-11:00 a.m. | 990 |
| 11:00-12:00 p.m. | 780 |

c) Explain different types of vertical deflection measures for traffic calming.
2. a) Design a two-phase signal at an isolated cross-junction for the following data:

Intergreen for N-S: 7 sec and E-W: 9 sec . Amber is 3 sec .
Lost time for starting and end delays : $4 \mathrm{sec}(\mathrm{N}-\mathrm{S})$ and $3 \mathrm{sec}(\mathrm{E}-\mathrm{W})$

|  | N | S | E | W |
| :--- | :---: | :---: | :---: | :---: |
| Flow(q), veh/hr | 950 | 860 | 670 | 780 |
| Saturation flow(s) veh/hr | 2750 | 2500 | 1870 | 2250 |

Assume any missing data. Draw bar diagram.
b) Briefly summarize the contribution of transportation for Cultural development and Economic development in Bangladesh.
c) A vehicle skids to a stop on a $5 \%$ upgrade initially traveling at $85 \mathrm{~km} / \mathrm{hr}$; taking 600 m to8 do so. Determine the coefficient of friction on this surface.
3. a) Explain the necessities of an effective bus terminal.
b) An accident evaluator predicts that a bus collided with a bridge pier at a speed of16 $23 \mathrm{mi} / \mathrm{hr}$. determined by her assessment of damage. After examination to the accident location she detected skid marks of 70 ft on the bituminous pavement ( $\mathrm{f}=0.425$ ) and 40 ft on the earth shoulder ( $\mathrm{f}=0.35$ ). There is $-2 \%$ grade. Determine the speed of the vehicle at the beginning of skid marks.
c) Compile the benefits of shoulders for highway design.
4. a) A sag vertical curve is to be designed to join a $-8 \%$ grade with a $+6 \%$ grade at a section of a two-lane highway. The design speed of the highway is 75 mph . Determine the minimum length of the curve. Assume the stopping sight distance is 800 ft .
b) A horizontal curve with a radius of 800 ft is designed for a two-lane highway having a design speed of 80 mph . If the section of highway have a $5 \%$ upgrade and coefficient of friction is 0.348 , estimate the least possible distance of any object can be placed from the
centerline of the inside lane of the curve. Assume PR time 2.5.
c) Explain "Cone of vision" and "Depth perception".
5. a) Spot speeds ( $\mathrm{km} / \mathrm{hr}$ ) of 50 vehicles navigating a section of an major road are as below: $43,86,54,43,67,66,36,68,67,72,69,78,57,47,63,65,49,56,58,52,55,67,63,48$, $77,42,83,37,55,38,55,37,39,32,57,46,73,56,43,37,47,44,68,53,67,64,66,46$, 49, 57.
Portray the design speed, average speed, safe speed, and median speed of speed.
(Consider pace as 10-19, 20-29 and so on)
b) Outline the factors influencing highway design.
6. a) Formulate briefly the various elements of Passing Sight Distance for a two-lane highway with figure.
b) An urban primary road with 75 ft pavement width having a reflectance of $11 \%$ carries a maximum of 2250 vph at night-time. Design the lighting system considering Sodium source with mounting height of 60 ft and a maintenance factor of 0.78 . Draw the lighting layout.

## Necessary equations:

$$
\begin{array}{ll}
S<L: & L=\frac{A S^{2}}{100\left(\sqrt{2 h_{1}}+\sqrt{2 h_{2}}\right)^{2}} \\
S>L: & L=2 S-\frac{200\left(\sqrt{h_{1}}+\sqrt{h_{2}}\right)^{2}}{A} \\
S<L: & L=\frac{A S^{2}}{200\left[2.0+S\left(\tan 1^{\circ}\right)\right]} \\
S>L: & L=2 S-\frac{200\left[2.0+S\left(\tan 1^{\circ}\right)\right]}{A}
\end{array}
$$

Table for Question 1 b)

Table 1 Hourly Expansion Factors for a Rural Primary Road

| Hour | Vol. | HEF | Hour | Vol. | HEF |
| :---: | ---: | ---: | :---: | ---: | :---: |
| 6:00-7:00 a.m. | 294 | 42.01 | 6:00-7:00 p.m. | 743 | 16.6 |
| 7:00-8:00 a a.m. | $426^{\circ}$ | 28.99 | 7:00-8:00 | p.m. | 706 |
| 17.5 |  |  |  |  |  |
| 8:00-9:00 a.m. | 560 | 22.05 | 8:00-9:00 p.m. | 606. | 20.4 |
| 9:00-10:00 a.m. | 657 | 18.8 | $9: 00-10: 00$ p.m. | 489 | 25.3 |
| 10:00-11:00 a.m. | 722 | 17.11 | 10:00-11:00 p.m. | 396 | 31.2 |
| 11:00-12:00 p.m. | 667 | 18.52 | 11:00-12:00 a.m. | 360 | 34.3 |
| 12:00-1:00 p.m. | 660 | 18.71 | $12: 00-1: 00$ a.m. | 241 | 51.2 |
| 1:00-2:00 p.m. | 739 | 16.71 | 1:00-2:00 a.m. | 150 | 82.3 |
| 2:00-3:00 p.m. | 832 | 14.84 | 2:00-3:00 a.m. | 100 | 124 |
| 3:00-4:00 p.m. | 836 | 14.77 | 3:00-4:00 a.m. | 90 | 137 |
| 4:00-5:00 p.m. | 961 | 12.85 | 4:00-5:00 a.m. | 86 | 144 |
| 5:00-6:00 p.m. | 892 | 13.85 | 5:00-6:00 a.m. | 137 | 90.2 |
| Total daily volume $=$ | 12350 |  |  |  |  |

Table 2 Daily Expansion Factors for a Rural Primary Road

| Day of Week | Volume | DEF |
| :---: | ---: | ---: |
| Sunday | 7,895 | 9.515 |
| Monday | 10,714 | 7.012 |
| Tuesday | 9,722 | 7.727 |
| Wednesday | 11,413 | 6.582 |
| Thusrday | 10,714 | 7.012 |
| Friday | 13,125 | 5.724 |
| Saturday | 11,539 | 6.51 |
| Total weekly volume $=$ | 75,122 |  |

Table for Question 6 b)
Table ! Recommended Average Lllumination (lumens/ft²)


Table 2 adustment Factors for recommended average Illumination values

| Surface Reflectance | Adjustment Factors |
| :---: | :---: |
| $3 \%$ or less | 1.5 |
| $10 \%$ | 1.0 |
| $20 \%$ or more | 0.75 |

Table 3 Lighting Source Characteristics

| Source Types | Expected Life <br> (hrs) | Lighting Efficiency <br> (Lumens/Watt) | Wattage <br> (Watt) |
| :--- | :---: | :---: | :---: |
| Tungsten | 1000 | $8-14$ | Up to 1000 |
| Fluorescent | 6000 | $50-75$ | Up to 250 |
| Sodium | 6000 | $100-120$ | Up to 160 |
| Mercury | 7500 | $20-60$ | Up to 400 |

TABLE 4 RECOMMENDED ARRANGEMENT OF STREET LIGHTING

| Type of Arrangement | Pavement Width |
| :--- | :--- |
| One side | Width $<=30 \mathrm{ft}$ |
| Both sides - Staggered | 30ft $>$ Width $<=60 \mathrm{ft}$ |
| Both sides - Opposite | Width $>60 \mathrm{ft}$ |

FIGURE 1 CO-EFFICIENT OF UTILIZATION CURVES (FOR LIGHT DISTRIBUTION TYPE III)


Note: Due to poor mainteriance, the actual co-efficient of utilization is reduced by a factor usually 0.8 (i.e. taken as $80 \%$ ).

# University of Asia Pacific <br> Department of Civil Engineering <br> Final Examination Spring 2018 <br> Program: B.Sc. Engineering (Civil) 



Figure No.: 1

1. $A, B, C, D, E, F$, and $G$ are the rain gauge station (shown in figure-1) having catchment area of 70 hectares of which $40 \%$ is covered with water surface. The latitude and elevation of the catchment area are $32^{\circ} 4^{\prime} \mathrm{N}$ and 230 m (above the sea level) from center of Bangladesh. Under catchment area, the water temperature is $25^{\circ} \mathrm{C}$, humidity is $60 \%$ and wind velocity at 2 m above ground is $22 \mathrm{~km} / \mathrm{h}$. Data are collected about 12 h sunshine period.

| Stations | $\mathbf{A}$ | $\mathbf{B}$ | $\mathbf{C}$ | $\mathbf{D}$ | $\mathbf{E}$ | $\mathbf{F}$ | $\mathbf{G}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Observed <br> precipitation(cm) | 43.5 | 30.5 | 42.3 | 29.9 | 20 | 45 | 25 |
| Area weighted factor | 0.31 | 0.20 | 0.07 | 0.10 | 0.05 | 0.15 | 0.12 |

Calculate the following:
i. Average rainfall in the catchment;
ii. Monthly evaporation;
iii. Weekly evapotranspiration;
iv. Infiltration ( $40 \%$ of avg. rainfall);
v. Losses (consider only interception losses);
vi. Total runoff.

2(a) Write short notes on (any two):
i. Application of Hydrology in civil engineering;
ii. Differentiate between convective and orographic storms;
iii. Form of precipitation;

2(b) In a diagram show (any two):
i. Formation of frontal cycle;
ii. Different routes of runoff;
iii. Water-budget method of evaporation;

2(c) The total river area of the world is $148.8 \mathrm{M} \mathrm{km}^{2}$ and has the water quantity $2.12 * 10^{3} \mathrm{~km}^{3}$. Assuming that all surface runoff to the oceans comes from rivers; calculate the average residence time of water in rivers.

|  | Unit | Ocean | Land |
| :---: | :---: | :---: | :---: |
| Precipitation | $\mathrm{Km}^{3} / \mathrm{yr}$ | 478,000 | 225,000 |
| Evaporation | $\mathrm{Km}^{3} / \mathrm{yr}$ | 596,000 | 725,000 |
| Atmospheric moisture | $\mathrm{Km}^{3} / \mathrm{yr}$ | 458,00 | 125,00 |

2(d) Calculate the precipitable water in a saturated air column extending 2 km up of $1 \mathrm{~m}^{2}$ ground surface. The surface pressure and air temperature are 101.3 kpa and $30^{\circ} \mathrm{C}$ respectively. The lapse rate is $6.5^{\circ} \mathrm{C} / \mathrm{km}$.

3(a) Write all factors that affect flood hydrograph.
3(b) The ordinates of a 6-h unit hydrograph of a catchment are given below:

| Time (h) | 0 | 4 | 8 | 12 | 16 | 20 | 24 | 32 | 40 | 48 | 56 | 64 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6-\mathrm{h} \mathrm{UH}$ | 0 | 20 | 35 | 49 | 85 | 115 | 190 | 168 | 105 | 45 | 20 | 0 |

Derive the flood hydrograph in the catchment due to storm given below:

| Time from start of storm (h) | 0 | 4 | 8 | 12 |
| :---: | :---: | :---: | :---: | :---: |
| Accumulated rainfall (cm) | 0 | 3 | 10 | 15 |

The storm loss rate for the catchment is estimated as $0.25 \mathrm{~cm} / \mathrm{h}$. The base flow can be assumed $20 \mathrm{~m}^{3} / \mathrm{s}$ at the beginning and increasing by $2 \mathrm{~m}^{3} / \mathrm{s}$ for every 12 hours till the end of direct runoff hydrograph.

3(c) Ordinates of a 4-h unit hydrograph are given below. Using given data derive the ordinates of a 2-h unit hydrograph for the same catchment.

| Time (h) | 0 | 4 | 8 | 12 | 16 | 20 | 24 | 28 | 32 | 36 | 40 | 44 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4-h UH | 0 | 20 | 80 | 130 | 150 | 130 | 90 | 52 | 25 | 15 | 5 | 0 |

4(a) Graphically define the attenuation and time lag of flood hydrograph.
4(b) The following inflow and outflow hydrographs were observed in a river reach. Estimate the value of $K$ and $x$ applicable to this reach for use in the Muskingum equation.

| Time $(\mathrm{h})$ | 0 | 4 | 8 | 12 | 16 | 20 | 24 | 28 | 32 | 36 | 40 | 44 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inflow $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | 5 | 18 | 45 | 45 | 30 | 20 | 15 | 10 | 8 | 7 | 6 | 6 |
| Outflow $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | 5 | 6 | 12 | 29 | 38 | 35 | 29 | 23 | 17 | 13 | 9 | 7 |

4(c) A reservoir has the following elevation, discharge and storage relationships:

| Elevation $(\mathrm{m})$ | 100 | 100.50 | 101 | 101.50 | 102 | 102.50 | 102.75 | 300 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Storage $\left(10^{6} \mathrm{~m}^{3}\right)$ | 3.34 | 3.48 | 3.55 | 3.88 | 4.39 | 4.85 | 5.48 | 5.90 |
| Discharge $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | 0 | 15 | 32 | 47 | 80 | 110 | 126 | 145 |

When the reservoir level was at 100.50 m , the following flood entered the reservoir.

| Time $(\mathrm{h})$ | 0 | 6 | 12 | 18 | 24 | 30 | 36 | 42 | 48 | 54 | 60 | 66 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Discharge $\left(\mathrm{m}^{3} / \mathrm{s}\right)$ | 12 | 24 | 54 | 82 | 76 | 56 | 45 | 32 | 40 | 21 | 15 | 13 |

Route the flood and obtain the outflow of the hydrograph.

5(a) What are the different methods to estimate the magnitude of a flood peak?
5(b) Flood-frequency computations for the Padma river at Mawa ghat, by using Gumbel's method, yielded the following results:

| Returns period, T (years) | Peak Flows $\left(\mathbf{m}^{\mathbf{3}} / \mathbf{s}\right)$ |
| :---: | :---: |
| 25 | 30,580 |
| 50 | 56,920 |
| 100 | 91,510 |

Estimate the flood magnitude in this river with a return period of 500 years.
5(c) Data covering a period of 95 years for the Jamuna river at Sirajgoaj yielded the mean and standard derivation of the annual flood series as $6450 \mathrm{~m}^{3} / \mathrm{s}$ and $3125 \mathrm{~m}^{3} / \mathrm{s}$ respectively. Using the Gumbel's method, estimate the flood discharge with a return period of 550 years. What are the (a) $95 \%$ and (b) $99 \%$ confidence limits for this estimate?

## Important equation and tables

$$
H_{n}=H_{a}(1-r)\left(a+b \frac{n}{N}\right)-\sigma T_{a}^{4}\left(0.56-0.092 \sqrt{e_{a}}\right)\left(0.10+0.90 \frac{n}{N}\right)
$$

| Surface | range of r values |
| :--- | ---: |
| Close ground crops | $0.15-0.25$ |
| Bare lands | $0.05-0.45$ |
| Water surface | $0.05-0.95$ |
| Snow | $0.45-0.95$ |

TAELE SATUAATION VAPOUR PRESSURE OF WATEA

| Temperature ( ${ }^{\circ}$ C) | Saturation vapour pressure ew (mm of Hes) | $\left.\mathrm{mm}^{\mathrm{A}} \mathrm{C}\right)$ |
| :---: | :---: | :---: |
| 0 | 4.58 | 0.30 |
| 5.0 | 6.54 | 0.45 |
| 7.5 | 7.78 | 0.54 |
| 10.0 | 9.21 | 0.60 |
| 12.5 | 10.87 | 0.71 |
| 15.0 | 12.79 | 0.80 |
| 17.5 | 15.00 | 0.95 |
| 20.0 | 17.54 | 1.05 |
| 22.5 | 20.44 | 1.24 |
| 25.0 | 23.76 | 1.40 |
| 27.5 | 27.54 | 1.61 |
| 30.0 | 31.82 | 1.85 |
| 32.5 | 36.68 | 2.07 |
| 35.0 | 42.81 | 2.35 |

TABLE MEAN MONTHLY SOLAR RADIATION AT TOP OF ATMOSPHERE, $H_{a}$ IN mm OF EVAPORABLE WATERJDAY

| North <br> lati <br> tude | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $0^{\circ}$ | 14.5 | 15.0 | 15.2 | 14.7 | 13.9 | 13.4 | 13.5 | 14.2 | 14.9 | 15.0 | 14.6 | 14.3 |
| $10^{\circ}$ | 12.8 | 13.9 | 14.8 | 15.2 | 15.0 | 14.8 | 14.8 | 15.0 | 14.9 | 14.1 | 13.1 | 12.4 |
| $20^{\circ}$ | 10.8 | 12.3 | 13.9 | 15.2 | 15.7 | 15.8 | 15.7 | 15.3 | 14.4 | 12.9 | 11.2 | 10.3 |
| $30^{\circ}$ | 8.5 | 10.5 | 12.7 | 14.8 | 16.0 | 16.5 | 16.2 | 15.3 | 13.5 | 11.3 | 9.1 | 7.9 |
| $40^{\circ}$ | 6.0 | 8.3 | 11.0 | 13.9 | 15.9 | 16.7 | 16.3 | 14.8 | 12.2 | 9.3 | 6.7 | 5.4 |
| $50^{\circ}$ | -3.6 | 5.9 | 9.1 | 12.7 | 15.4 | 16.7 | 16.1 | 13.9 | 10.5 | 7.1 | 4.3 | 3.0 |

TABLE
MEAN MONTHLY VALUES OF POSSIBLE SUNSHINE HOURS, $N$

| North <br> lati <br> ruce | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $0^{\circ}$ | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 | 12.1 |
| $10^{\circ}$ | 11.6 | 11.8 | 12.1 | 12.4 | 12.6 | 12.7 | 12.6 | 12.4 | 12.9 | 11.9 | 11.7 | 11.5 |
| $20^{\circ}$ | 11.1 | 11.5 | 12.0 | 12.6 | 13.1 | 13.3 | 13.2 | 12.8 | 12.3 | 11.7 | 11.2 | 10.9 |
| $30^{\circ}$ | 10.4 | 11.1 | 12.0 | 12.9 | 13.7 | 14.1 | 13.9 | 13.2 | 12.4 | 11.5 | 10.6 | 10.2 |
| $40^{\circ}$ | 9.6 | 10.7 | 11.9 | 13.2 | 14.4 | 15.0 | 14.7 | 13.8 | 12.5 | 11.2 | 10.0 | 9.4 |
| $50^{\circ}$ | 8.6 | 10.1 | 11.8 | 13.8 | 15.4 | 16.4 | 16.0 | 14.5 | 12.7 | 10.8 | 9.1 | 8.1 |



TAGLE 7.3 REDUCED MEAN In IN GUMEEL'S EXTREME VALUE DISTRIBUTION
$N=$ sample size

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 0.4952 | 0.4996 | 0.5035 | 0.5070 | 0.5100 | 0.5128 | 0.5157 | 0.5181 | 0.5202 | 0.5220 |
| 20 | 0.5236 | 0.5252 | 0.5268 | 0.5283 | 0.5296 | 0.5309 | 0.5320 | 0.5332 | 0.5343 | 0.5353 |
| 30 | 0.5362 | 0.5371 | 0.53880 | 0.5388 | 0. 5396 | 0.5402 | 0.5410 | 0.5418 | 0.5424 | 0.5430 |
| 40 | 0.5436 | 0.5442 | 0.5.448 | 0.5453 | 0.5458 | 0.5463 | 0.5468 | 0.5473 | 0.5477 | 0.5481 |
| 50 | 0.5485 | 0.5489 | 0.5493 | 0.5497 | 0. 5501 | 0.5504 | 0.5508 | 0.5511 | 0.ssis | 0.5518 |
| 60 | 0.5521 | 0.5524 | 0.5527 | 0.5530 | 0.5533 | 0.5535 | 0.5538 | 0.5540 | 0.5543 | 0.5345 |
| 70 | 0.5548 | 0.5550 | 0.5552 | 0.5355 | 0.5357 | 0.5559 | 0.5361 | 0.5563 | 0.5565 | 0.3567 |
| 80 | 0.5569 | 0.5570 | 0.5572 | 0.5374 | 0.5576 | 0.5578 | 0.55880 | 0.5581 | 0.5583 | 0.5585 |
| 90 | 0.5586 | 0.5587 | 0.5589 | 0.5591 | 0.5592 | 0.5593 | c.ssss | 0.5596 | 0.5398 | 0.5599 |
| 100 | 0.5600 |  |  |  |  |  |  |  |  |  |

TABLE 7.4 REDUCED STANDAFD DEVIATION SI IN GUMBEL'S EXTREME VALUE DISTRIEUTION
$N=$ sample size

| N | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 0.9496 | 0.9676 | 0.9833 | 0.9971 | 1.0095 | 1.0206 | 1.0316 | 1.0511 | 1.0493 | 1.0565 |
| 20 | 1.0628 | 1.0696 | 1.0754 | $1.081^{\circ}$ | 1.0864 | 1.0915 | 1.0961 | 1.1004 | 1.1047 | 1.1086 |
| 30 | 1.1124 | 1.1159 | 1.1193 | 1.1226 | 1.1255 | 1.1285 | 1.1313 | 1. 1339 | 1.1363 | 1.1388 |
| 40 | 1.1413 | 1.1436 | 1.1458 | 1.1480 | 1.1499 | 1.1519 | 1.1538 | 1.1557 | 1.1574 | 1. 1590 |
| so. | 1.1607 | 1.1623 | 1.1638 | 1.1658 | 1.1667 | . 1.1681 | 1.1696 | 1.1708 | 1.1721 | 1.1734 |
| 60 | 1.1747 | 1.1759 | 1.1770 | 1.1782 | 1.1793 | 1.1803 | 1.1814 | 1. 1824 | 1.1834 | 1.1844 |
| 70 | 1.1854 | 1.1863 | 6.1873 | 1.1881 | 1.1890 | 1.1898 | 1.1906 | 1.1915 | 1.1923 | 1.1930 |
| 80 | 1.1938 | 1.1945 | 1.1953 | 1.1959 | 1.1967 | 1.1973 | 1.1980 | 1.1987 | 1.1994 | 1.2001 |
| 90 | 1.2007 | 1. 2013 | 1. 2020 | 1.2026 | 1.2032 | 1.2038 | 1.2044 | 1.20.49 | 1.2055 | 1.2060 |
| 100 | 1.20065 |  |  |  |  |  |  |  |  |  |

# University of Asia Pacific Department of Civil Engineering <br> Final Examination Spring 2018 <br> Program: B.Sc in Civil Engineering 

Course Title: Principles of Management
Course Code: IMG 301
Time: 2 hrs.
(Answer any four of the following questions.)

1. (a) Write four actions that companies aiming for a blue ocean strategy should consider. ..... 5
(b) What is Delphi technique? Describe the process of Delphi technique. ..... 10
(c) Describe formal and informal organization. ..... 10
2. Explain the bases of power and empowerment policy with examples. ..... 25
3. Write about organization culture. ..... 25
4. Describe personal characteristics that a manager should possess. ..... 25
5. Evaluate Maslow's hierarchy of needs theory of motivation. ..... 25
